The Virial Equations I

We can obtain an important tensor equation relating global properties of the system, by multiplying the CBE by both v_j and x_k and then integrating over the entire phase-space.

The first step of this has already been performed in our derivation of the Jeans equations, and yielded the momentum equations

$$rac{\partial (
ho \langle v_j
angle)}{\partial t} + rac{\partial (
ho \langle v_i v_j
angle)}{\partial x_i} +
ho rac{\partial \Phi}{\partial x_j} = 0$$

Multiplying all terms with $\boldsymbol{x}_{\boldsymbol{k}}$ and integrating over real space yields

$$rac{\partial}{\partial t}\int
ho x_k\langle v_j
angle \mathrm{d}^3x=-\int x_krac{\partial(
ho\langle v_iv_j
angle)}{\partial x_i}\mathrm{d}^3ec x-\int
ho\, x_k\,rac{\partial\Phi}{\partial x_j}\mathrm{d}^3ec x$$

Using integration by parts the first term on the r.h.s. becomes

$$egin{array}{rll} \int x_k rac{\partial (
ho \langle v_i v_j
angle)}{\partial x_i} \mathrm{d}^3 ec x &=& \int rac{\partial (
ho x_k \langle v_i v_j
angle)}{\partial x_i} \mathrm{d}^3 ec x - \int
ho \langle v_i v_j
angle rac{\partial x_k}{\partial x_i} \mathrm{d}^3 ec x &=& -\int \delta_{ki}
ho \langle v_i v_j
angle \mathrm{d}^3 ec x &=& -\int \rho \langle v_k v_j
angle \mathrm{d}^3 ec x &=& -\int
ho \langle v_k v_j
angle \mathrm{d}^3 ec x &=& -\int \rho \langle v_k v_j
angle \mathrm{d}^3 ec x &=& -2 \mathcal{K}_{kj} \end{array}$$

where we have defined the kinetic energy tensor

 $\mathcal{K}_{ij} = rac{1}{2} \int
ho \langle v_i v_j
angle \mathrm{d}^3 ec{x}$

The Virial Equations II

It is customary to split the kinetic energy tensor into contributions from ordered and random motions:

$$\mathcal{K}_{ij}\equiv\mathcal{T}_{ij}+rac{1}{2}\Pi_{ij}$$

where

$$\mathcal{T}_{ij} \equiv rac{1}{2} \int
ho ig \langle v_i
angle \, \mathrm{d}^3 ec x$$
 $\Pi_{ij} \equiv \int
ho \, \sigma_{ij}^2 \, \mathrm{d}^3 ec x$

In addition to the \mathcal{K} we also define the potential energy tensor

$$\mathcal{W}_{ij}\equiv -\int
ho x_i rac{\partial \Phi}{\partial x_j} \mathrm{d}^3ec{x}$$

Combining the above we obtain

$$rac{\partial}{\partial t}\int
ho\, x_k \langle v_j
angle \mathrm{d}^3 x = 2\mathcal{K}_{kj} + \mathcal{W}_{kj}$$

which allows us to write

$$rac{1}{2}rac{\mathrm{d}}{\mathrm{d}t}\int
ho\left[x_k\left\langle v_j
ight
angle+x_j\left\langle v_k
ight
angle
ight]=2\mathcal{K}_{jk}+\mathcal{W}_{jk}$$

where we have used that \mathcal{K} and \mathcal{W} are symmetric.

The Virial Equations III

Finally we also define the moment of inertia tensor

 ${\cal I}_{ij}\equiv\int
ho\,x_i\,x_j\,{
m d}^3ec x$

Differentiating with respect to time, and using the continuity equation (i.e., the zeroth moment equation of the CBE) yields

$$\begin{array}{lll} \frac{\mathrm{d} I_{jk}}{\mathrm{d} t} &=& \int \frac{\partial \rho}{\partial t} x_j \, x_k \, \mathrm{d}^3 \vec{x} \\ &=& -\int \frac{\partial \rho \langle v_i \rangle}{\partial x_i} x_j \, x_k \, \mathrm{d}^3 \vec{x} \\ &=& -\int \frac{\partial (\rho \langle v_i \rangle x_j x_k)}{\partial x_i} \mathrm{d}^3 \vec{x} + \int \rho \langle v_i \rangle \frac{\partial (x_j x_k)}{\partial x_i} \mathrm{d}^3 \vec{x} \\ &=& \int \rho \langle v_i \rangle \left[x_j \delta_{ik} + x_k \delta_{ij} \right] \mathrm{d}^3 \vec{x} \\ &=& \int \rho \left[x_j \langle v_k \rangle + x_k \langle v_j \rangle \right] \mathrm{d}^3 \vec{x} \end{array}$$

so that

$$rac{1}{2}rac{\mathrm{d}}{\mathrm{d}t}\int
ho\left[x_kig\langle v_jig
angle+x_jig\langle v_kig
angle
ight]=rac{1}{2}rac{\mathrm{d}^2\mathcal{I}_{jk}}{\mathrm{d}t^2}$$

which allows us to write the Tensor Virial Theorem as

$$rac{1}{2}rac{\mathrm{d}^2 \mathcal{I}_{jk}}{\mathrm{d}t^2} = 2\mathcal{T}_{jk} + \Pi_{jk} + \mathcal{W}_{jk}$$

which relates the gross kinematic and structural properties of gravitational systems.

The Virial Equations IV

If the system is in a steady-state the moment of inertia tensor is stationary, and the Tensor Virial Theorem reduces to $2\mathcal{K}_{ij} + \mathcal{W}_{ij} = 0$.

Of particular interest is the trace of the Tensor Virial Theorem, which relates the total kinetic energy $K = \frac{1}{2}M\langle v^2 \rangle$ to the total potential energy $W = \frac{1}{2}\int \rho(\vec{x}) \Phi(\vec{x}) d^3\vec{x}.$

$$\begin{aligned} \operatorname{tr}(\mathcal{K}) &\equiv \sum_{i=1}^{3} \mathcal{K}_{ii} &= \frac{1}{2} \int \rho(\vec{x}) \left[\langle v_{1}^{2} \rangle(\vec{x}) + \langle v_{2}^{2} \rangle(\vec{x}) + \langle v_{3}^{2} \rangle(\vec{x}) \right] \mathrm{d}^{3} \vec{x} \\ &= \frac{1}{2} \int \rho(\vec{x}) \langle v^{2} \rangle(\vec{x}) \mathrm{d}^{3} \vec{x} \\ &= \frac{1}{2} M \langle v^{2} \rangle = K \end{aligned}$$

where we have used that

$$\langle v^2
angle = rac{1}{M} \int
ho(ec x) \langle v^2
angle(ec x) \mathrm{d}^3 ec x$$

Similarly, the trace of the potential energy tensor is equal to the total potential energy (see next page for derivation):

 $\operatorname{tr}(\mathcal{W}) = W = rac{1}{2} \int
ho(ec{x}) \, \Phi(ec{x}) \, \mathrm{d}^3 ec{x}$

We thus obtain the scalar virial theorem

$$2K+W=0$$

The Potential Energy Tensor I

We have defined the potential energy tensor as

$$\mathcal{W}_{ij}\equiv -\int
ho x_i rac{\partial \Phi}{\partial x_j} \mathrm{d}^3ec{x}$$

Using that $\Phi(ec{x}) = -G \int rac{
ho(ec{x})}{|ec{x}'-ec{x}|} \mathrm{d}^3 ec{x}$ we obtain

$$\mathcal{W}_{ij} = G \int \int
ho(ec{x}) \,
ho(ec{x}') rac{x_i(x_j'-x_j)}{|ec{x}'-ec{x}|^3} \mathrm{d}^3ec{x}' \mathrm{d}^3ec{x}$$

Using that \vec{x} and \vec{x}' are dummy variables, we may relabel them, and write

$$\mathcal{W}_{ij} = G \int \int
ho(ec{x}') \,
ho(ec{x}) rac{x_j'(x_k-x_k')}{|ec{x}-ec{x}'|^3} \mathrm{d}^3ec{x}\mathrm{d}^3ec{x}'$$

Interchanging the order of integration and summing the above two equations yields the manifestly symmetric expression

$$\mathcal{W}_{ij} = -rac{G}{2} \int \int
ho(ec{x}) \,
ho(ec{x'}) rac{(x'_j - x_j)(x'_k - x_k)}{|ec{x'} - ec{x}|^3} \mathrm{d}^3 ec{x'} \mathrm{d}^3 ec{x}$$

This expression allows us to write

$$\begin{split} \mathrm{tr}(\mathcal{W}) &\equiv \sum_{i=1}^{3} \mathcal{W}_{ii} = -\frac{G}{2} \int \int \rho(\vec{x}) \rho(\vec{x}') \frac{|\vec{x}' - \vec{x}|^2}{|\vec{x}' - \vec{x}|^3} \mathrm{d}^3 \vec{x}' \mathrm{d}^3 \vec{x} \\ &= -\frac{G}{2} \int \rho(\vec{x}) \int \frac{\rho(\vec{x}')}{|\vec{x}' - \vec{x}|} \mathrm{d}^3 \vec{x}' \mathrm{d}^3 \vec{x} = \frac{1}{2} \int \rho(\vec{x}) \Phi(\vec{x}) \mathrm{d}^3 \vec{x} = W \end{split}$$

The Surface Pressure Term

In our derivation on the previous pages we obtained

$$\int x_k \frac{\partial (\rho \langle v_i v_j \rangle)}{\partial x_i} \mathrm{d}^3 \vec{x} = \int \frac{\partial (\rho x_k \langle v_i v_j \rangle)}{\partial x_i} \mathrm{d}^3 \vec{x} - \int \rho \langle v_i v_j \rangle \frac{\partial x_k}{\partial x_i} \mathrm{d}^3 \vec{x} \\ = -\int \rho \langle v_k v_j \rangle \mathrm{d}^3 \vec{x} = -2\mathcal{K}_{kj}$$

where we have used that

$$\int rac{\partial (
ho x_k \langle v_i v_j
angle)}{\partial x_i} \mathrm{d}^3 ec x = \int
ho x_k \langle v_k v_j
angle \mathrm{d}^2 S = 0$$

based on the assumption that $\rho(r) = 0$ when $r \to \infty$. However, this is only true for an isolated system with 'vacuum' boundary conditions.

In reality, a halo or galaxy is embedded in a cosmological density field, often with ongoing infall. This yields a non-zero surface pressure. In its most general form the scalar virial theorem therefore reads

$$2K + W + S_p = 0$$

with the surface pressure term

$$S_p = -\int \langle v^2
angle ec r \cdot ec n \mathrm{d}^2 ec S$$

As long as $S_p \neq 0$ we thus expect that $2K/|W| \neq 1$. See Shapiro et al. (astro-ph/0409173) for a detailed discussion.

The Virial Equations V

From a simple dimensional analysis one finds that $|W| \propto GM^2/R$ with M the system's mass and R a characteristic radius.

A useful characteristic radius is the so-called gravitational radius defined by

$$r_g \equiv rac{GM^2}{|W|}$$

One can relate the gravitational radius to the half-mass radius r_h , defined as radius enclosing half the total mass. As shown by Spitzer (1969), typical stellar systems have $r_g \simeq 2.5 r_h$.

Combining this with the scalar virial theorem we can write that

$$M\simeq 2.5rac{r_h\langle v^2
angle}{G}$$

which is a useful equation to obtain a (rough) estimate of the virial mass from a measure of the half-mass radius and the rms motion

The Virial Equations VI

Using the scalar virial theorem we obtain

$$E = K + W = -K = \frac{1}{2}W$$

Consider the formation of a virialized object. If the system forms by collecting material from large radii, the initial conditions are well approximated by $K_{\text{init}} = W_{\text{init}} = E_{\text{init}} = 0$.

Because of gravity the matter starts to collapse. Since $W = -GM^2/r_g$ this makes W more negative. At the same time K increases. Initially, during the early collapse, E = T + W = 0.

After the first shell crossing, the system starts to virialize. When virialization is complete, 2T + W = 0 and E = W/2.

Therefore, half the gravitational energy released by collapse is invested in kinetic form. The system somehow disposes of the other half in order to achieve a binding energy $E_b = -E$.

QUESTION Where does the other half of the energy go?

Application: M/L of Spherical Systems

As an application of the Virial Theorem, consider spherical, non-rotating systems (spherical galaxies or globulars)

If the mass-to-light ratio Υ does not depend on radius then

 $K_{xx} = \int rac{1}{2}
ho(ec{x}) \langle v_x^2
angle \mathrm{d}^3 ec{x} = rac{\Upsilon}{2} \int
u(ec{x}) \langle v_x^2
angle \mathrm{d}^3 ec{x}$

where $\nu(\vec{x}) = \rho(\vec{x})/\Upsilon$ is the 3D luminosity distribution, and K_{xx} is the kinetic energy associated with motion in the *x*-direction

Since a spherical, non-rotating system is isotropic we have that

$$K = K_{xx} + K_{yy} + K_{zz} = 3K_{xx}$$

If one has observationally determined the surface brightness profile $\Sigma(R)$ and the line-of-sight velocity dispersion $\sigma_p^2(R)$ then it is easy to see that

$$K = 3\frac{\Upsilon}{2} \int_{0}^{2\pi} \mathrm{d}\phi \int_{0}^{\infty} \mathrm{d}RR\Sigma(R)\sigma_{p}^{2}(R) = 3\pi\Upsilon \int_{0}^{\infty} \mathrm{d}RR\Sigma(R)\sigma_{p}^{2}(R) \equiv \Upsilon J$$

where we defined the observationally accessible $J=J(\Sigma,\sigma_p^2)$

Application: M/L of Spherical Systems

As seen in exersizes, for spherical system:

$$W=-rac{G}{2}\int\limits_{0}^{\infty}rac{M^2(r)}{r^2}\mathrm{d}r$$

Using that $M(r) = 4\pi \int_{0}^{r} \rho(r') r'^2 \mathrm{d}r'$

where the density profile is related to $\Sigma(R)$ according to

$$ho(r)=-rac{\Upsilon}{\pi}\int\limits_{r}^{\infty}rac{\mathrm{d}\Sigma}{\mathrm{d}R}rac{\mathrm{d}R}{\sqrt{R^2-r^2}}$$

we obtain that

$$W = -8 \Upsilon^2 \int\limits_0^\infty rac{\mathrm{d}r}{r^2} \left[\int\limits_0^r \mathrm{d}r' \, r'^2 \int\limits_{r'}^\infty rac{\mathrm{d}\Sigma}{\mathrm{d}R} rac{\mathrm{d}R}{\sqrt{R^2 - r^2}}
ight]^2 \equiv \Upsilon^2 ilde{J}$$

where we have defined the observationally accessible integral $ilde{J} = ilde{J}(\Sigma)$

According to the virial theorem 2K + W = 0, and thus -2K/W = 1. Substituting $K = \Upsilon J$ and $W = \Upsilon^2 \tilde{J}$ we thus obtain that

$$\Upsilon = -rac{2J}{ ilde{J}}$$

Flattening of Oblate Spheroids I

As another application of the virial theorem we relate the flattening of an oblate spheroid to its kinematics.

Consider an oblate system with it's symmetry axis along the z-direction. Because of symmetry considerations we have that

$$\langle v_R
angle = \langle v_z
angle = 0 \qquad \quad \langle v_R v_\phi
angle = \langle v_z v_\phi
angle = 0$$

If we write that

$$\langle v_{m{x}}
angle = \langle v_{\phi}
angle \sin \phi \qquad \quad \langle v_{m{y}}
angle = \langle v_{\phi}
angle \cos \phi$$

we obtain

$$\begin{aligned} \mathcal{T}_{xy} &= \frac{1}{2} \int \rho \langle v_x \rangle \langle v_y \rangle \mathrm{d}^3 \vec{x} \\ &= \frac{1}{2} \int _0^{2\pi} \mathrm{d}\phi \sin \phi \, \cos \phi \, \int _0^{\infty} \mathrm{d}R \int _{-\infty}^{\infty} \mathrm{d}z \rho(R,z) \langle v_\phi \rangle^2(R,z) \\ &= 0 \end{aligned}$$

A similar analysis shows that all other non-diagonal elements of \mathcal{T} , Π , and \mathcal{W} have to be zero.

In addition, because of symmetry considerations we must have that $\mathcal{T}_{xx} = \mathcal{T}_{yy}, \Pi_{xx} = \Pi_{yy}$, and $\mathcal{W}_{xx} = \mathcal{W}_{yy}$.

Flattening of Oblate Spheroids II

Given these symmetries, the only independent, non-trivial virial equations are

 $2\mathcal{T}_{xx}+\Pi_{xx}+\mathcal{W}_{xx}=0, \qquad \qquad 2\mathcal{T}_{zz}+\Pi_{zz}+\mathcal{W}_{zz}=0$

Taking the ratio we find that

$$rac{2\mathcal{T}_{xx}+\Pi_{xx}}{2\mathcal{T}_{zz}+\Pi_{zz}}=rac{\mathcal{W}_{xx}}{\mathcal{W}_{zz}}$$

The usefulness of this equation lies in the fact that, for density distributions that are constant on similar concentric spheroids, i.e., $\rho = \rho(m^2)$, the ratio $\mathcal{W}_{xx}/\mathcal{W}_{zz}$ depends only on the axis ratio c/a of the spheroids, and is independent of the density profile! For an oblate body, to good approximation

$$rac{\mathcal{W}_{xx}}{\mathcal{W}_{zz}}\simeq \left(rac{\mathrm{c}}{a}
ight)^{-0.9}$$

Let us start by considering isotropic, oblate rotators.

Then $\Pi_{xx}=\Pi_{zz}=M ilde{\sigma}^2$, $\mathcal{T}_{zz}=0$ and $\mathcal{T}_{xx}+\mathcal{T}_{yy}=2\mathcal{T}_{xx}=rac{1}{2}M ilde{v}^2$.

Here M is the total mass, $\tilde{\sigma}^2$ is the mass-weighted rms-average of the intrinsic one-dimensional velocity dispersion, and \tilde{v}^2 is the mass-weighted rms rotation velocity.

Flattening of Oblate Spheroids III

Thus, for an isotropic, oblate rotators we have that

$$rac{rac{1}{2}M ilde{v}^2+M ilde{\sigma}^2}{M ilde{\sigma}^2}\simeq ig(rac{c}{a}ig)^{-0.9}$$

which reduces to

$$rac{ ilde{v}}{ ilde{\sigma}}\simeq \sqrt{2[(c/a)^{-0.9}-1]}$$

This specifies the relation between the flattening of the spheroid and the ratio of streaming motion to random motion. Note that you need a rather large amount of rotation to achieve only modest flattening: c/a = 0.7 requires $\tilde{v} \sim 0.9\tilde{\sigma}$

Next consider a non-rotating, anisotropic, oblate system:

In this case $\Pi_{xx} = M \tilde{\sigma}_{xx}^2$ and $\Pi_{zz} = M \tilde{\sigma}_{zz}^2$, and the virial theorem gives that

$$rac{ ilde{\sigma}_{zz}}{ ilde{\sigma}_{xx}} \simeq \left(rac{c}{a}
ight)^{0.45}$$

Now a flattening of c/a=0.7 requires only a small anisotropy of $ilde{\sigma}_{zz}/ ilde{\sigma}_{xx}\simeq 0.85$

Flattening of Oblate Spheroids IV

Finally, consider the general case of rotating, anisotropic, oblate systems Now we have $\Pi_{zz} = (1 - \delta)\Pi_{xx} = (1 - \delta)M\tilde{\sigma}^2$, $\mathcal{T}_{zz} = 0$ and $2\mathcal{T}_{xx} = \frac{1}{2}M\tilde{v}^2$, where we have introduced the anistropy parameter $\delta < 1$.

In this case the virial theorem gives

$$rac{ ilde{v}}{ ilde{\sigma}}\simeq \sqrt{2[(1-\delta)\,(c/a)^{-0.9}-1]}$$

This shows that observations of $\tilde{v}/\tilde{\sigma}$ and the ellipticity $\varepsilon = 1 - (c/a)$ allow us to test whether elliptical galaxies are supported by rotation or by anisotropic pressure.

A potential problem is that we can not directly measure \tilde{v} nor $\tilde{\sigma}$. Rather, we measure properties that are projected along the line-of-sight. Furthermore, in general we don't see a system edge-on but under some unknown inclination angle i. Note that i also affects the measured v and σ . As shown in Binney & Tremaine, the overall effect is to move a point on the oblate rotator line mainly along that line.

Flattening of Oblate Spheroids V



Observations reveal a dichotomy: luminous ellipticals are supported by anisotropic pressure, while fainter ellipticals (and bulges) are consistent with being oblate, isotropic rotators.

NOTE: If luminous ellipticals are anisotropic, there is no good reason why they should be axisymmetric: massive ellipticals are triaxial

The Jeans Theorem I

RECALL: An integral of motion is a function $I(\vec{x}, \vec{v})$ of the phase-space coordinates that is constant along all orbits, i.e.,

 $\frac{\mathrm{d}I}{\mathrm{d}t} = \frac{\partial I}{\partial x_i} \frac{\mathrm{d}x_i}{\mathrm{d}t} + \frac{\partial I}{\partial v_i} \frac{\mathrm{d}v_i}{\mathrm{d}t} = \vec{v} \cdot \vec{\nabla}I - \vec{\nabla}\Phi \cdot \frac{\partial I}{\partial \vec{v}} = 0$

Compare this to the CBE for a steady-state (static) system:

$$ec v \cdot ec
abla f - ec
abla \Phi \cdot rac{\partial f}{\partial ec v} = 0$$

Thus the condition for I to be an integral of motion is identical with the condition for I to be a steady-state solution of the CBE. Hence:

Jeans Theorem Any steady-state solution of the CBE depends on the phase-space coordinates only through integrals of motion. Any function of these integrals is a steady-state solution of the CBE.

PROOF: Let f be any function of the n integrals of motion $I_1, I_2, ... I_n$ then

$$rac{\mathrm{d}f}{\mathrm{d}t} = \sum\limits_{k=1}^n rac{\partial f}{\partial I_k} rac{\mathrm{d}I_k}{\mathrm{d}t} = 0$$

which proofs that f satisfies the CBE.

The Jeans Theorem II

More useful than the Jeans Theorem is the Strong Jeans Theorem, which is due to Lynden-Bell (1962).

Strong Jeans Theorem The DF of a steady-state system in which almost all orbits are regular can be written as a function of the independent isolating integrals of motion, or of the action-integrals.

Note that a regular orbit in a system with n degrees of freedom is uniquely, and completely, specified by the values of the n isolating integrals of motion in involution. Thus the DF can be thought of as a function that expresses the probability for finding a star on each of the phase-space tori.

We first consider an application of the Jeans Theorem to Spherical Systems As we have seen, any orbit in a spherical potential admits four isolating integrals of motion: E, L_x, L_y, L_z .

Therefore, according to the Strong Jeans Theorem, the DF of any[†] steady-state spherical system can be expressed as $f = f(E, \vec{L})$.

* except for point masses and uniform spheres, which have five isolating integrals of motion

Jeans Theorem & Spherical Systems

If the system is spherically symmetric in all its properties, then $f = f(E, L^2)$ rather than $f = f(E, \vec{L})$: i.e., the DF can only depend on the magnitude of the angular momentum vector, not on its direction.

Contrary to what one might naively expect, this is **not** true in general. In fact, as beautifully illustrated by Lynden-Bell (1960), a spherical system **can** rotate without being oblate.

Consider a spherical system with $f(E, \vec{L}) = f(E, -\vec{L})$. In such a system, for each star S on a orbit \mathcal{O} , there is exactly one star on the same orbit \mathcal{O} but counterrotating with respect to S. Consequently, this system is perfectly spherically symmetric in all its properties.

Now consider all stars in the z = 0-plane, and revert the sense of all those stars with $L_z < 0$. Clearly this does not influence $\rho(r)$, but it does give the system a net sense of rotation around the *z*-axis.

Thus, although a system with $f = f(E, L^2)$ is not the most general case, systems with $f = f(E, \vec{L})$ are rarely considered in galactic dynamics.

Isotropic Spherical Models I

An even simpler case to consider is the one in which f = f(E).

Since $E=\Phi(ec{r})+rac{1}{2}[v_r^2+v_ heta^2+v_\phi^2]$ we have that

$$egin{aligned} &\langle v_r^2
angle &=rac{1}{
ho}\int \mathrm{d} v_r\mathrm{d} v_ heta\mathrm{d} v_\phi\,v_r^2\,f\left(\Phi+rac{1}{2}[v_r^2+v_ heta^2+v_\phi^2]
ight)\ &\langle v_ heta^2
angle &=rac{1}{
ho}\int \mathrm{d} v_r\mathrm{d} v_ heta\mathrm{d} v_\phi\,v_ heta^2\,f\left(\Phi+rac{1}{2}[v_r^2+v_ heta^2+v_\phi^2]
ight)\ &\langle v_\phi^2
angle &=rac{1}{
ho}\int \mathrm{d} v_r\mathrm{d} v_ heta\mathrm{d} v_\phi\,v_\phi^2\,f\left(\Phi+rac{1}{2}[v_r^2+v_ heta^2+v_\phi^2]
ight) \end{aligned}$$

Since these equations differ only in the labelling of one of the variables of integration, it is immediately evident that $\langle v_r^2 \rangle = \langle v_{\theta}^2 \rangle = \langle v_{\phi}^2 \rangle$.

Assuming that f = f(E) is identical to assuming that the system is isotropic

Note that from

$$\langle v_i
angle = rac{1}{
ho} \int \mathrm{d} v_r \mathrm{d} v_{ heta} \mathrm{d} v_{\phi} \, v_i \, f \left(\Phi + rac{1}{2} [v_r^2 + v_{ heta}^2 + v_{\phi}^2]
ight)$$

it is also immediately evident that $\langle v_r \rangle = \langle v_\theta \rangle = \langle v_\phi \rangle = 0$. Thus, similar as for a system with $f = f(E, L^2)$ a system with f = f(E) has no net sense of rotation.

Isotropic Spherical Models II

In what follows we define the relative potential $\Psi \equiv -\Phi + \Phi_0$ and relative energy $\mathcal{E} = -E + \Phi_0 = \Psi - \frac{1}{2}v^2$. In general one chooses Φ_0 such that f > 0 for $\mathcal{E} > 0$ and f = 0 for $\mathcal{E} \le 0$

Now consider a self-consistent, spherically symmetric system with $f = f(\mathcal{E})$. Here self-consistent means that the potential is due to the system itself, i.e.,

$$abla^2 \Psi = -4\pi G
ho = -4\pi G \int f(\mathcal{E}) \mathrm{d}^3 ec v$$

(note the minus sign in the Poisson equation), which can be written as

$$rac{1}{r^2}rac{\mathrm{d}}{\mathrm{d}r}\left(r^2rac{\mathrm{d}\Psi}{\mathrm{d}r}
ight)=-16\pi^2G\int\limits_0^\Psi f(\mathcal{E})\,\sqrt{2(\Psi-\mathcal{E})}\,\mathrm{d}\mathcal{E}$$

Note: Here we have chosen Φ_0 so that $\Psi(r \to \infty) = 0$. In systems with infinite total mass, such as the logarithmic potential or the isothermal sphere, the system is more conveniently normalized such that $\Psi(r \to \infty) = -\infty$. In that case $\int_0^{\Psi} d\mathcal{E}$ needs to be replace by $\int_{-\infty}^{\Psi} d\mathcal{E}$.

Isotropic Spherical Models III

This relation may be regarded either as non-linear equation for $\Psi(r)$ given $f(\mathcal{E})$, or as linear equation for $f(\mathcal{E})$ given $\Psi(r)$.

"from
$$ho$$
 to f "

As an example, consider a stellar-dynamical system with a DF

$$f(\mathcal{E}) = rac{
ho_1}{(2\pi\sigma_0^2)^{3/2}} \exp\left(rac{\Psi - rac{1}{2}v^2}{\sigma_0^2}
ight)$$

The corresponding density is

$$ho(\Psi) = 4\pi \int_{0}^{\sqrt{2\Psi}} f(\mathcal{E}) v^2 \mathrm{d}v = 4\pi \int_{0}^{\Psi} f(\mathcal{E}) \sqrt{2(\Psi - \mathcal{E})} \mathrm{d}\mathcal{E} =
ho_1 \mathrm{e}^{\Psi/\sigma_0^2}$$

The Poisson equation reads

$$\tfrac{1}{r^2} \tfrac{\mathrm{d}}{\mathrm{d}r} \left(r^2 \tfrac{\mathrm{d}\Psi}{\mathrm{d}r} \right) = -4\pi G \rho_1 \mathrm{e}^{\Psi/\sigma_0^2} \quad \Rightarrow \quad \tfrac{\mathrm{d}\Psi}{\mathrm{d}r} = - \tfrac{4\pi G \rho_1}{r^2} \int\limits_0^r r^2 \mathrm{e}^{\Psi/\sigma_0^2} \mathrm{d}r$$

Inspection shows that the solution for $\Psi(r)$ and the corresponding ho(r) are

$$\Psi(r)=-2\sigma_0^2{
m ln} r \qquad
ho(r)=rac{\sigma_0^2}{2\pi Gr^2}$$

which is the potential-density pair of a singular isothermal sphere.

Isotropic Spherical Models IV

Note that the DF of the singular isothermal sphere implies that

$$f(v) \propto {
m e}^{-rac{v^2}{2\sigma_0^2}}$$

which is identical to a Maxwell-Boltzmann distribution, if we set $\sigma_0^2 = \frac{k_B T}{m}$. Therefore, the structure of a singular isothermal sphere is identical to that of an isothermal self-gravitating sphere of gas.

The isothermal nature of this system becomes evident if we consider the Jeans equation. For a system with $f = f(\mathcal{E})$ there is only one non-trivial Jeans equation:

$$\frac{1}{\rho} \frac{\mathrm{d}\rho\sigma^2}{\mathrm{d}r} = \frac{\mathrm{d}\Psi}{\mathrm{d}r}$$

where $\sigma^2\equiv\langle v_r^2
angle=\langle v_{ heta}^2
angle=\langle v_{\phi}^2
angle.$

Substituting the expressions for ho and Ψ this yields

$$\sigma^2(r)=\sigma_0^2$$

thus the local velocity dispersion, which is related to the "temperature", is independent of r.

Eddington's Formula

"from f to ho"

Using that Ψ is a monotonic function of r, so that ρ can be regarded as a function of Ψ , we have

$$ho(\Psi) = \int f \mathrm{d}^3 ec{v} = 4\pi \int \limits_0^\Psi f(\mathcal{E}) \sqrt{2(\Psi-\mathcal{E})} \mathrm{d}\mathcal{E}$$

differentiating both sides with respect to Ψ yields

$$rac{1}{\sqrt{8}\pi}rac{\mathrm{d}
ho}{\mathrm{d}\Psi}=\int\limits_{0}^{\Psi}rac{f(\mathcal{E})\,\mathrm{d}\mathcal{E}}{\sqrt{\Psi-\mathcal{E}}}$$

which is an Abel integral equation, whose solution is

$$f(\mathcal{E}) = rac{1}{\sqrt{8}\pi^2} rac{\mathrm{d}}{\mathrm{d}\mathcal{E}} \int \limits_0^{\mathcal{E}} rac{\mathrm{d}
ho}{\mathrm{d}\Psi} rac{\mathrm{d}\Psi}{\sqrt{\mathcal{E}-\Psi}}$$

This is called **Eddington's formula**, which may also be written in the form

$$f(\mathcal{E}) = rac{1}{\sqrt{8}\pi^2} \left[egin{smallmatrix} \mathcal{E} \ \int \ d^2
ho \ d\Psi^2 \ \sqrt{\mathcal{E}-\Psi} + rac{1}{\sqrt{\mathcal{E}}} \left(rac{\mathrm{d}
ho}{\mathrm{d}\Psi}
ight)_{\Psi=0}
ight]$$

Eddington's Formula

Given a spherically symmetric density distribution, which can be written as $\rho = \rho(\Psi)$ (which is not always possible), Eddington's formula yields a corresponding DF $f = f(\mathcal{E})$.

Note, however, that there is no guarantee that the solution for $f(\mathcal{E})$ satisfies the physical requirement that $f \ge 0$ for all \mathcal{E} .

Using Eddington's formula

$$f(\mathcal{E}) = rac{1}{\sqrt{8}\pi^2} rac{\mathrm{d}}{\mathrm{d}\mathcal{E}} \int \limits_0^{\mathcal{E}} rac{\mathrm{d}
ho}{\mathrm{d}\Psi} rac{\mathrm{d}\Psi}{\sqrt{\mathcal{E}-\Psi}}$$

we see that the requirement $f(\mathcal{E}) \geq 0$ is identical to the the requirement that the function

$$\int\limits_{0}^{\mathcal{E}}rac{\mathrm{d}
ho}{\mathrm{d}\Psi}rac{\mathrm{d}\Psi}{\sqrt{\mathcal{E}\!-\!\Psi}}$$

is an increasing function of \mathcal{E} .

If a density distribution $\rho(r)$ does not satisfy this requirement, then the model obtained by setting the anisotropy parameter $\beta = 0$ [i.e., by assuming that $f = f(\mathcal{E})$] and solving the Jeans Equations is unphysical.

Anisotropic Spherical Models I

In the more general case, spherical systems (with spherical symmetry in all their properties) have $f = f(E, L^2)$.

These models are anisotropic, in that $\langle v_r^2 \rangle \neq \langle v_{\theta}^2 \rangle = \langle v_{\phi}^2 \rangle$.

Anisotropic spherical models are non-unique: many different $f(E, L^2)$ can correspond to a given $\rho(r)$ and $\Psi(r)$. These models differ, though, in their dynamic properties. No equivalent of the Edddington Formula thus exists, that allows to compute $f(E, L^2)$ given $\rho(r)$.

Additional assumptions need to be made. For example, Kent & Gunn (1982) discussed models with $f(E, L^2) = g(E)L^{-2\beta}$, which have a constant anisotropy, i.e., $\beta(r) = \beta$.

An other example are the so called Osipkov-Merritt models (Osipkov 1979; Merritt 1985) were the assumption is made that $f(E, L^2) = f(Q)$ with

$$Q = \mathcal{E} - rac{L^2}{2r_a^2}$$

Here r_a is the so-called anisotropy radius.

Anisotropic Spherical Models II

The usefulness of the Osipkov-Merritt models becomes apparent from

$$ho_Q(r) \equiv \left(1+rac{r^2}{r_a^2}
ight)
ho(r) = 4\pi\int\limits_0^\Psi f(Q)\sqrt{2(\Psi-Q)}\mathrm{d}Q$$

Thus $[\rho_Q(r), f(Q)]$ are similarly related as $[\rho(r), f(\mathcal{E})]$ so that we may use Eddington's formula to write

$$f(Q) = rac{1}{\sqrt{8}\pi^2} rac{\mathrm{d}}{\mathrm{d}Q} \int \limits_0^Q rac{\mathrm{d}
ho_Q}{\mathrm{d}\Psi} rac{\mathrm{d}\Psi}{\sqrt{Q-\Psi}}$$

For Osipkov-Merritt models one can show that

$$eta(r)=rac{r^2}{r^2+r_a^2}$$

Thus, these models are isotropic for $r \ll r_a$, become radially anisotropic at around r_a , and become competely radial at large r.

Since purely radial orbits contribute density at the center, models with constant density cores can only have DFs of the Osipkov-Merritt form, i.e., $f = f(E, L^2) = f(Q)$, for sufficiently large r_a . Alternatively, if r_a is relatively small, the (self-consistent) $\rho(r)$ needs to have a central cusp.

Anisotropic Spherical Models III

Next we consider the family of **Quasi-Separable** DFs (Gerhard 1991):

$$f(\mathcal{E}, L^2) = g(\mathcal{E}) h(x)$$
 $x = rac{L}{L_0 + L_c(\mathcal{E})}$

with L_0 a constant, and $L_c(\mathcal{E})$ the angular momentum of the circular orbit with energy \mathcal{E} .

Here $g(\mathcal{E})$ controls the distribution of stars between energy surfaces, while the circularity function h(x) describes the distribution of stars over orbits of different angular momenta on surfaces of constant \mathcal{E} .

Depending on the choise for h(x) one can construct models with different anisotropies. If h(x) decreases with increasing x, the model will be radially anisotropic, and vice versa.

Once a choise for h(x) is made, one can (numerically) obtain $g(\mathcal{E})$ for a given $\rho(r)$.

All these various models are useful to explore how different orbital anisotropies impact on observables, such as the line-of-sight velocity distributions (LOSVDs).

Anisotropic Spherical Models IV



Velocity profiles, $\mathcal{L}(v)$, for the outer parts of spherical $f(E, L^2)$ models. Results are shown for $\beta = \infty$ (circular orbits), -1, 0 (isotropic model), 0.5, and 1 (radial orbits). The unit of velocity is the velocity dispersion, which is different for each curve. (from: van der Marel & Franx 1993)

Velocity profiles are not expected to be Gaussian

Spherical Models: Summary I

In its most general form, the DF of a static, spherically symmetric model has the form $f = f(E, \vec{L})$. From the symmetry of individual orbits one can see that one always has to have

$$\langle v_r
angle = \langle v_ heta
angle = 0 \qquad \quad \langle v_r v_\phi
angle = \langle v_r v_ heta
angle = \langle v_ heta v_\phi
angle = 0$$

This leaves four unknowns: $\langle v_{\phi} \rangle$, $\langle v_{r}^{2} \rangle$, $\langle v_{\theta}^{2} \rangle$, and $\langle v_{\phi}^{2} \rangle$

If one makes the assumption that the system is spherically symmetric in all its properties then $f(E, \vec{L}) o f(E, L^2)$ and

$$\langle v_{\phi}
angle = 0 \qquad \quad \langle v_{ heta}^2
angle = \langle v_{\phi}^2
angle$$

In this case the only non-trivial Jeans equation is

$$rac{1}{
ho} rac{\partial (
ho \langle v_r^2
angle)}{\partial r} + 2 rac{eta \langle v_r^2
angle}{r} = -rac{\mathrm{d} \Phi}{\mathrm{d} r}$$

with the anisotropy parameter defined by

$$eta(r) = 1 - rac{\langle v_r^2
angle(r)}{\langle v_r^2
angle(r)}$$

Spherical Models: Summary II

Many different models, with different orbital anisotropies, can correspond to the same density distribution. Examples of models are:

- $f(E, L^2) = f(E)$
- $f(E, L^2) = g(E)\delta(L)$
- $f(E, L^2) = g(E)\delta[L L_c(E)]$
- $f(E, L^2) = g(E)L^{-2\beta}$
- $f(E, L^2) = f(E + L^2/2r_c^2)$

isotropic model, i.e., $\beta = 0$ radial orbits only, i.e. $\beta = 1$ circular orbits only, i.e., $oldsymbol{eta}=-\infty$ constant anisotropy, i.e. $\beta(r) = \beta$ • $f(E, L^2) = g(E)h(L)$ anisotropy depends on circularity function h

center isotropic, outside radial

Suppose I have measured the surface brightness profile $\Sigma(R)$ and the line-of-sight velocity dispersion $\sigma_p^2(R)$. Depending on the assumption regarding $\beta(r)$ these data imply very different mass distributions M(r). One can (partially) break this mass-anisotropy degeneracy by using information regarding the LOSVD shapes.